

GUÍA DE TRABAJOS PRACTICO
BASE CON COLUMNA EMPOTRAI

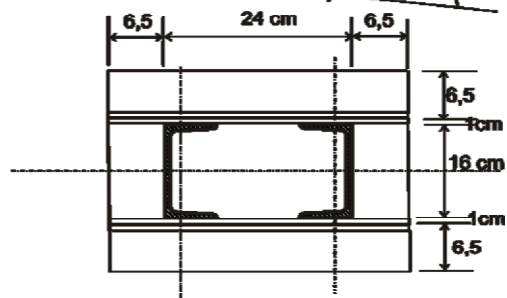
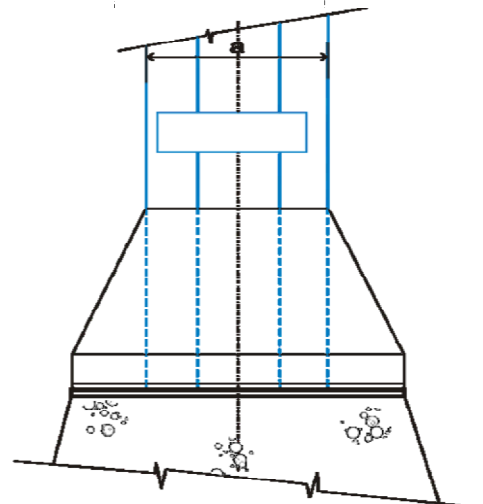
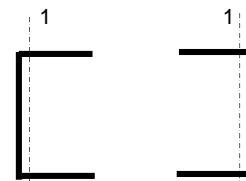
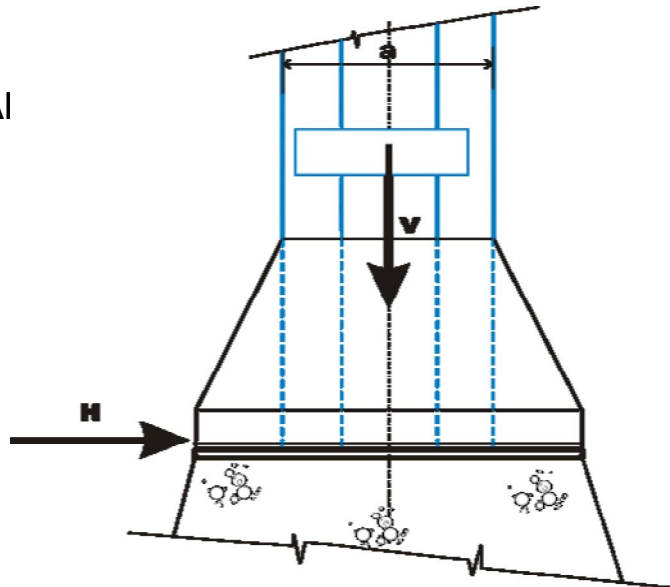
DATOS:

- V = 5,90 t
- H = 2,30 t
- M = 2000 kgm
- e = 33,9 cm
- $\sigma_{H^0} = 40 \text{ kg/cm}^2$
- $\sigma_t = 1 \text{ kg/cm}^2$
- $\gamma_{H^0} = 2,40 \text{ t/m}^3$
- $\gamma_{tr} = 1,60 \text{ t/m}^3$

(AC 3.3.2.4.3.)

Sección de columna = 2 PNU 160
a = 24 cm

- $\Gamma = 48 \text{ CIII}$
- $I_x = 1850 \text{ cm}^4$
- $W_x = 232 \text{ cm}^3$
- $i_x = 6,21 \text{ cm}$
- $i_1 = 1,89 \text{ cm}$
- $e_y = 1,84 \text{ cm}$
- $I_y = 5130 \text{ cm}^4$
- $W_y = 428 \text{ cm}^3$
- $i_y = 10,3 \text{ cm}$



$$* \sigma = \frac{V}{a_1 * b_1} \leq \dots$$

$$** \sigma = \frac{V}{a_1 * b_1} + \frac{M}{(a_1 * b_1^2)}$$

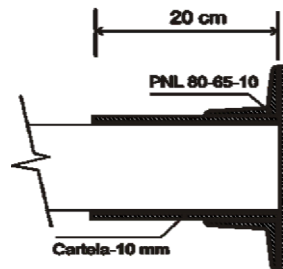
adopto $a_1 = a + 2 \text{ PNL}$

$$* b_1 = \frac{5900 \text{ kg}}{30 \text{ kg/cm}^2 * 3}$$

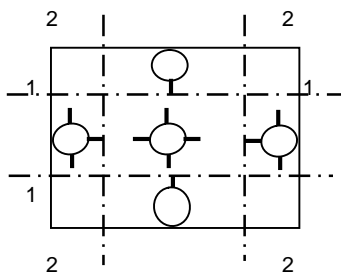
adopto $b_1 = 16 \text{ cm}$ (PNL)

$$** \sigma_{trab} = \frac{5900}{31 * 37} + \frac{2}{31}$$

$$q_{tr} = 33,42 \text{ kg/cm}^2$$



CALCULO DE PLACA INFERIOR Ó DE ASIEN TO



Determinación de momentos considerando placas (losas)

s/eje 1-1

$$M_1 = \frac{q \cdot l_1^2}{2} = 706 \text{ kgcm/cm}$$

s/eje 2-2

$$M_2 = 706 \text{ kgcm/cm}$$

Losa central

$$M_3 \text{ ap y } \begin{array}{|c|} \hline \square \\ \hline \end{array} = -595 \text{ kgcm/cm}$$

$$M_3 \text{ tr y } \begin{array}{|c|} \hline \square \\ \hline \end{array} = 602 \text{ kgcm/cm}$$

Dimensionado

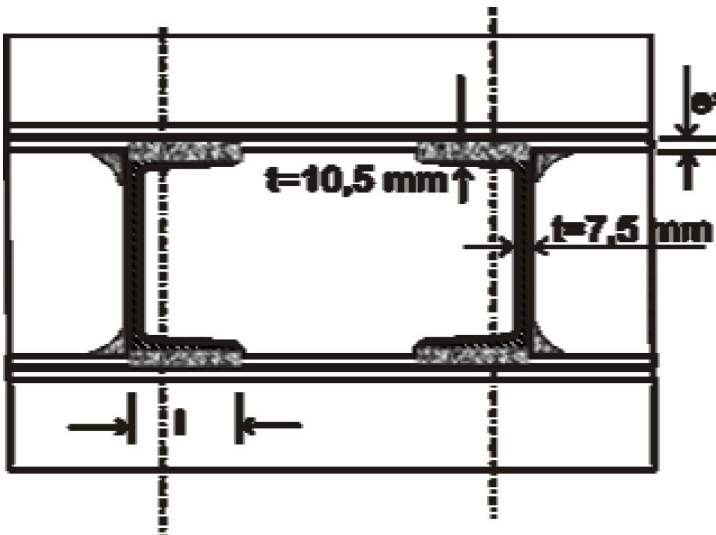
Acero F24
Clase II
Destino C
Cargas P S
 $\gamma = 1,45$

} $\sigma_{adm} = 1.665 \text{ kg/cm}^2$

de $\sigma = \frac{M}{W} = \frac{M_1}{l_{cm} \cdot e^2 / 6} \leq \sigma_{adm} \implies t_{nec} = \sqrt{\frac{706 \cdot \text{kgcm} \cdot 6}{1665 \text{ kg/cm}^2 \cdot 1\text{cm}}}$

$t_{nec} = 1,59 \text{ cm}$
Adopto $t = 19,0 \text{ mm}$ (3/4")

CALCULO DE UNIONES SOLDADAS



ncho soldadura $\left\{ \begin{array}{l} > 0,3 \text{ mm} \\ < 0,7 t_{min} = 0,7 \text{ mm} \end{array} \right.$

N VERTICAL CARTELA-PERFIL U

$$\frac{V}{2 \cdot n=2} + \frac{M}{a \cdot n=2} = 5.641 \text{ kg}$$

$$= \frac{F}{a_s \cdot l} \leq \tau_{adm} = 1245 \text{ kg/cm}^2$$

$\implies I_{nec} \left\{ \begin{array}{l} < \frac{F}{0.3 \cdot 1245} = 15 \text{ cm} \\ > \frac{F}{0.7 \cdot 1245} = 6.47 \text{ cm} \end{array} \right. \quad I_{sold} = I_{nec} + 2a = 15,6 \text{ cm}$

$I_{sold} = I_{nec} + 2a = 7,87 \text{ cm}$

$I_{sold} \left\{ \begin{array}{l} > 15 a_{min} = 4,5 \text{ cm} \\ < 60 a = 42 \text{ cm} \end{array} \right.$

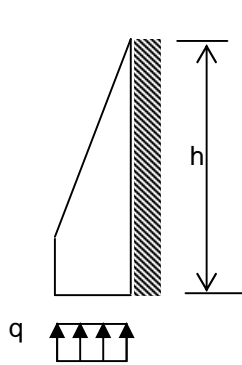
adopto $I_{sold} = 8 \text{ cm}$

UNION HORIZONTAL CARTELA-PERFIL U

$a_s = 0,7 \text{ cm}$

$l = \frac{H}{4 * a_s * \tau_{adm}} = 1,54 \text{ cm}$ **adopto** $l_{sold} = 6 \text{ cm}$

VERIFICACION DE LA CARTELA



$q = q_{tr} * 31 \text{ cm} / 2 = 518 \text{ kg/cm}$

se considera como una ménsula corta:

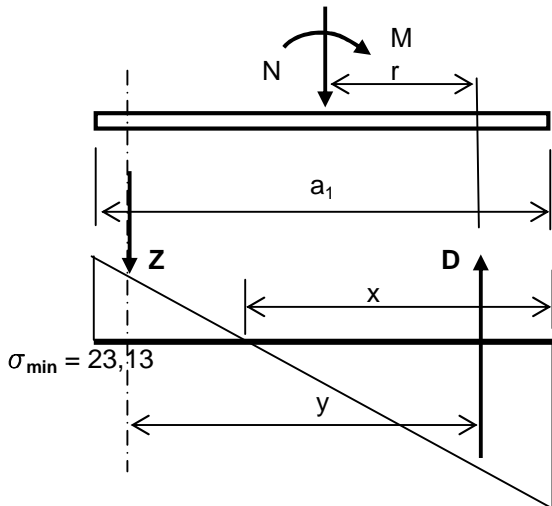
$M = \frac{q * l^2}{2} = \frac{518 * 6.5^2 \text{ cm}^2}{2} = 10.943 \text{ kgcm}$

se adopta $t = 10 \text{ mm}$

$\frac{M}{W} = \frac{10943 \text{ kgcm}}{\frac{t * h^2}{6}} \leq \sigma_{adm} \implies h_{nec} = 6,28 \text{ cm}$

se adopta $h = 20 \text{ cm}$ (constructivo)

CALCULO DE PERNOS DE ANCLAJE



$\frac{x}{a_1} = \frac{\sigma_{max}}{|\sigma_{max}| + |\sigma_{min}|}$

$\sigma_{max;min} = \frac{N}{A} \left(1 \pm \frac{6 * e}{a_1} \right) = \begin{cases} \sigma_{min} = 23,13 \\ \sigma_{max} = -33,39 \end{cases}$

$e = 33,9 \text{ cm}$

$x = 21,85 \text{ cm}$

$y = 2/3 a_1 = 24,67 \text{ cm}$

Se debe considerar la situación más desfavorable, que es el caso hipotético de que $N = 0$ y sólo esté actuando el M

$Z = M/y = 200000 \text{ kgcm} / 24,67 \text{ cm} = 8.107 \text{ kg}$

Si está actuando $N = 5.900 \text{ kg}$ $r = a/2 - x/3 = 11,22 \text{ cm}$

$\sum M_D = 0 \implies Z = \frac{M - N * r}{y} = \frac{200.000 - 5.900 * 11.22}{24.67} = 5.424 \text{ kg}$

$A_{nec} = \frac{Z}{n * \sigma_{adm}} = \frac{8.107 \text{ kg}}{3 * 1.665 \text{ kg/cm}^2} = 1.63 \text{ cm}^2$

$\Phi_{nec} = 1,43 \text{ cm} / ,87 = 1,63 \text{ cm}$

adopto $\Phi_{perno} = 1,6 \text{ cm}$ (5/8") verifica también para la situación de $N=5.900 \text{ kg}$

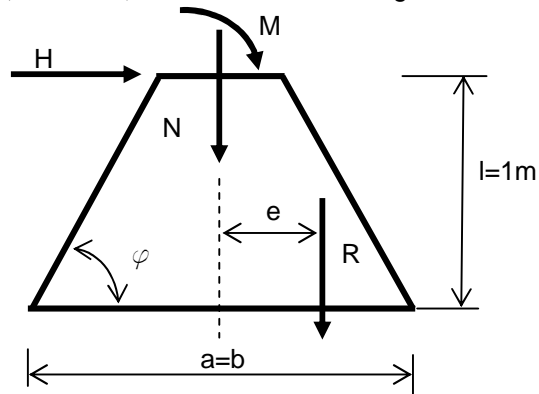
$l_{anclaje} = \frac{Z}{n * \pi * \phi * \tau_{adm}} = \frac{8.107 \text{ kg}}{3 * 3,14 * 1,6 * 6 \text{ kg/cm}^2} = 90 \text{ cm} > 10\Phi = 16 \text{ cm}$

$$n^{\circ} \pi^{\circ} \phi^{\circ} \tau_{adm} \quad 3 * 3,14 * 1,6 * 6.kg/cm^2$$

CALCULO DE LA BASE DE HORMIGÓN

$$R = N + B + T = 5900 \text{ kg} + (\text{vol } T * \gamma_t) + (\text{vol } h^{\circ} * \gamma_{h^{\circ}}) = 13.100 \text{ kg}$$

$$\begin{aligned} \gamma_t &= 1.600 \text{ kg/m}^3 \\ \text{Vol}_t &= 2,4 \text{ m}^3 \quad \text{estimado} \\ \gamma_{h^{\circ}} &= 2.400 \text{ kg/m}^3 \\ \text{Vol}_{h^{\circ}} &= 1,4 \text{ m}^3 \quad \text{estimado} \end{aligned}$$



es conveniente que las tensiones sobre el terreno sean positivas inferiores a la admisible.

$$e = \frac{H * d + M}{R} = \frac{(2.300 * 1m) + 2.000kgm}{13.100.kg} = 0,33 \text{ m} \quad \Rightarrow \quad a = b = 2m$$

$$\sigma_{1-2} = \frac{R}{a * b} \left(1 \pm \frac{6 * e}{a}\right) = \begin{cases} \sigma_1 = 0,65 \text{ kg/cm}^2 \\ \sigma_2 = 0,003 \text{ kg/cm}^2 \end{cases}$$

se deben verificar las siguientes condiciones constructivas:

1) el ángulo de talud debe ser $> 50^{\circ}$ por ser hormigón simple

$$\phi = \arctg 100 / \frac{(200 - 37)}{2} =$$

$$\phi = 50,8^{\circ} \text{ (BC)}$$

2) la altura de la base debe ser mayor a ala longitud de anclaje del perno $l > 90 \text{ cm}$ (se adopta $l = 100 \text{ cm}$)